## NAVAL ARCHITECTURE <br> $\qquad$

Attempt SIX questions only

## All questions carry equal marks

## Marks for each part question are shown in brackets

1. A ship of length 120 m displaces 10650 tonne when floating at a draught of 7.2 m in sea water of density $1025 \mathrm{~kg} / \mathrm{m}^{3}$. The waterplane area is defined by half breadths as given in Table Q1.

| Station | AP | $1 / 2$ | 1 | 2 | 3 | 4 | 5 | 6 | 7 | $71 / 2$ | FP |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $1 / 2$ Breadth (m) | 0 | 3.0 | 6.0 | 7.0 | 9.0 | 9.0 | 9.0 | 7.0 | 4.0 | 2.0 | 0 |
| Table Q1 |  |  |  |  |  |  |  |  |  |  |  |

When a mass of 10 tonne is moved a distance of 16 m across the deck, a deflection of 40 mm is recorded on a pendulum of 8 m length.

The height of the centre of buoyancy above the keel (KB) may be determined using Morrish's formula as given below.

$$
\mathrm{KB}=\left(\frac{5}{6} \times d\right)-\left(\frac{\nabla}{3 \times \mathrm{A}_{w}}\right)
$$

Calculate the KG of the ship in the above condition.
2. A ship of length 150 m and breadth 20 m floats upright at a draught of 7.5 m in sea water of density $1025 \mathrm{~kg} / \mathrm{m}^{3}$ and the height of the centre of gravity above the keel (KG) is 5.388 m .

Further hydrostatic data for this condition are as follows:

| centre of buoyancy above the keel $(\mathrm{KB})$ | $=3.956 \mathrm{~m}$ |
| :--- | :--- |
| height of metacentre above the keel $(\mathrm{KM})$ | $=7.014 \mathrm{~m}$ |
| waterplane area coefficient $\left(\mathrm{C}_{\mathrm{w}}\right)$ | $=0.82$ |
| block coefficient $\left(\mathrm{C}_{\mathrm{b}}\right)$ | $=0.72$ |

In the above condition there is an empty rectangular wing tank 16 m long, 5 m wide and 5 m deep, adjacent to the hull and directly above a double bottom tank 1.2 m deep.

Calculate the angle to which the ship will heel when the tank is completely filled with fresh water of density $1000 \mathrm{~kg} / \mathrm{m}^{3}$, assuming the ship to be wall sided over the change of draught.
3. The hydrostatic particulars given in Table Q3 are for a ship of length 150 m when floating in water of density $1025 \mathrm{~kg} / \mathrm{m}^{3}$.

| Draught <br> $(\mathrm{m})$ | Displacement <br> (tonne) | MCT I cm <br> $(\mathrm{tm})$ | LCB from <br> midships $(\mathrm{m})$ | LCF from <br> midships $(\mathrm{m})$ |
| :---: | :---: | :---: | :---: | :---: |
| 7.5 | 18200 | 216.5 | 0.85 forward | 2.44 aft |
| 7.0 | 16800 | 214.0 | 1.07 forward | 2.24 aft |
| Table Q3 |  |  |  |  |

The ship floats in water of density $1015 \mathrm{~kg} / \mathrm{m}^{3}$ with draughts of 7.6 m aft and 6.8 m forward.

Calculate EACH of the following:
(a) the displacement;
(b) the longitudinal position of the ship's centre of gravity.
4. A ship of 10000 tonne displacement has a rudder area of $25 \mathrm{~m}^{2}$. The ship has a KM of $6.9 \mathrm{~m}, \mathrm{KG}$ of 6.3 m and the centre of lateral resistance is 3.9 m above the keel.

The maximum rudder angle is 35 degrees and the centroid of the rudder is 2.3 m above the keel.

The force generated normal to the plane of the rudder is given by:

$$
\mathrm{F}=590 \mathrm{~A} v^{2} \sin \alpha
$$

Where: $A=$ rudder area
$\mathrm{v}=$ ship speed in $\mathrm{m} / \mathrm{s}$
$a=$ rudder helm angle
Calculate EACH of the following, when the ship is travelling at 22 knots:
(a) the angle and direction of heel due to the rudder force only, if it is put hard over to port;
(b) the angle and direction of heel due to the combination of centrifugal force and rudder force when the rudder is hard over to port and the vessel turns in a circle of 800 m diameter.
5. For a ship 120 m in length and 16 m breadth, the draught is 7 m in sea water of density $1025 \mathrm{~kg} / \mathrm{m}^{3}$ and the block coefficient is 0.7 .

The effective power (naked) of the ship at a speed of 14 knots is estimated at 1900 kW .

$$
\text { wetted surface area }\left(\mathrm{m}^{2}\right) \quad=\quad 2.57 \sqrt{\Delta L}
$$

Calculate the pull required to tow a similar model of length 4.8 m at the corresponding speed in fresh water of density $1000 \mathrm{~kg} / \mathrm{m}^{3}$.

Note: The frictional coefficient for the model in fresh water is 1.703
The frictional coefficient for the ship in sea water is 1.421
Speed in $\mathrm{m} / \mathrm{s}$ with index ( $n$ ) for ship and model 1.825
6. The ship data in Table Q6 have been derived from the results of model experiments:

| Ship speed (knots) | 14 | 15 | 16 |
| :---: | :---: | :---: | :---: |
| Effective power (kW) | 2620 | 3380 | 4580 |
| Thrust deduction fraction | 0.196 | 0.192 | 0.186 |
| Taylor wake fraction | 0.305 | 0.300 | 0.297 |
| Propeller efficiency | 0.685 | 0.695 | 0.690 |

Table Q6
Determine EACH of the following using the data in Table Q6:
(a) the ship speed when the propeller is absorbing 5050 kW delivered power;
(b) the propeller speed (rev/sec) given that the propeller has a diameter of 6 m with a pitch ratio of 0.85 and is operating at a real slip of $34 \%$.
7. (a) With reference to ship hull vibration, explain, with the aid of diagrams, EACH of the following terms:
(i) two-node vertical mode;
(ii) three-node horizontal mode;
(b) State how hull vibration can be minimised in vessels during the design stage and on vessels already built.

